

Designation: 71S1/97

# Standard Test Method for **Kinematic Viscosity of Transparent and Opaque Liquids** (the Calculation of Dynamic Viscosity)<sup>1</sup>

This standard is issued under the fixed designation D 445; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reapproval. A superscript epsilon  $(\epsilon)$  indicates an editorial change since the last revision or reapproval.

This test method has been approved by the sponsoring committee and accepted by the Cooperating Societies in accordance with established procedures.

This standard has been approved for use by agencies of the Department of Defense.

### 1. Scope

1.1 This test method specifies a procedure for the determination of the kinematic viscosity,  $\nu$ , of liquid petroleum products, both transparent and opaque, by measuring the time for a volume of liquid to flow under gravity through a calibrated glass capillary viscometer. The dynamic viscosity, n, can be obtained by multiplying the kinematic viscosity,  $\nu$ , by the density,  $\rho$ , of the liquid.

Note 1—For the measurement of the kinematic viscosity and viscosity of bitumens, see also Test Methods D 2170 and D 2171.

- 1.2 The result obtained from this test method is dependent upon the behavior of the sample and is intended for application to liquids for which primarily the shear stress and shear rates are proportional (Newtonian flow behavior). If, however, the viscosity varies significantly with the rate of shear, different results may be obtained from viscometers of different capillary diameters. The procedure and precision values for residual fuel oils, which under some conditions exhibit non-Newtonian behavior, have been included.
- 1.3 The range of kinematic viscosities covered by this test method is from 0.2 to 300 000 mm<sup>2</sup>/s (see Table A1.1) at all temperatures (see 6.3 and 6.4). The precision has only been determined for those materials, kinematic viscosity ranges and temperatures as shown in the footnotes to the precision section.
- 1.4 The values stated in SI units are to be regarded as the standard.
- 1.5 This standard does not purport to address all of the safety concerns, if any, associated with its use. It is the

responsibility of the user of this standard to establish appropriate safety and health practices and determine the applicability of regulatory limitations prior to use.

#### 2. Referenced Documents

- 2.1 ASTM Standards:
- D 446 Specifications and Operating Instructions for Glass Capillary Kinematic Viscometers<sup>2</sup>
- D 1193 Specification for Reagent Water<sup>3</sup>
- D 1217 Test Method for Density and Relative Density (Specific Gravity) of Liquids by Bingham Pycnometer<sup>2</sup>
- D 1480 Test Method for Density and Relative Density (Specific Gravity) of Viscous Materials by Bingham Pycnometer<sup>2</sup>
- D 1481 Test Method for Density and Relative Density (Specific Gravity) of Viscous Materials by Lipkin Bicapillary Pycnometer<sup>2</sup>
- D 2170 Test Method for Kinematic Viscosity of Asphalts (Bitumens)<sup>4</sup>
- D 2171 Test Method for Viscosity of Asphalts by Vacuum Capillary Viscometer<sup>4</sup>
- D 6074 Guide for Characterizing Hydrocarbon Lubricant Base Oils<sup>5</sup>
- E 1 Specification for ASTM Thermometers<sup>6</sup>
- E 77 Test Method for the Inspection and Verification of Thermometers<sup>6</sup>
- 2.2 ISO Standards:<sup>7</sup>
- ISO Guide 25—General Requirements for the Calibration and Testing Laboratories

<sup>&</sup>lt;sup>1</sup> This test method is under the jurisdiction of ASTM Committee D-2 on Petroleum Products and Lubricants and is the direct responsibility of Subcommittee D02.07 on Flow Properties.

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In the IP, this test method is under the jurisdiction of the Standardization Committee.

<sup>&</sup>lt;sup>2</sup> Annual Book of ASTM Standards, Vol 05.01.

<sup>&</sup>lt;sup>3</sup> Annual Book of ASTM Standards, Vol 11.01.

<sup>&</sup>lt;sup>4</sup> Annual Book of ASTM Standards, Vol 04.03.

<sup>&</sup>lt;sup>5</sup> Annual Book of ASTM Standards, Vol 05.03.

<sup>&</sup>lt;sup>6</sup> Annual Book of ASTM Standards, Vol 14.03.

<sup>&</sup>lt;sup>7</sup> Available from American National Standards Institute, 11 W. 42nd St., 13th Floor, New York, NY 10036.



- ISO 3104 Petroleum Products—Transparent and Opaque Liquids—Determination of Kinematic Viscosity and Calculation of Dynamic Viscosity
- ISO 3105 Glass Capillary Kinematic Viscometers— Specification and Operating Instructions
- ISO 3696 Water for Analytical Laboratory Use— Specification and Test Methods
- ISO 9000 Quality Management and Quality Assurance Standards—Guidelines for Selection and Use

# 3. Terminology

- 3.1 Definitions of Terms Specific to This Standard:
- 3.1.1 *density*, *n*—the mass per unit volume of a substance at a given temperature.
- 3.1.2 *dynamic viscosity*, *n*—the ratio between the applied shear stress and rate of shear of a liquid.
- 3.1.2.1 *Discussion*—It is sometimes called the coefficient of dynamic viscosity or, simply, viscosity. Thus dynamic viscosity is a measure of the resistance to flow or deformation of a liquid.
- 3.1.2.2 *Discussion*—The term dynamic viscosity can also be used in a different context to denote a frequency-dependent quantity in which shear stress and shear rate have a sinusodial time dependence.
- 3.1.3 *kinematic viscosity*, *n*—the resistance to flow of a fluid under gravity.
- 3.1.3.1 *Discussion*—For gravity flow under a given hydrostatic head, the pressure head of a liquid is proportional to its density,  $\rho$ . For any particular viscometer, the time of flow of a fixed volume of fluid is directly proportional to its kinematic viscosity,  $\nu$ , where  $\nu = \eta/\rho$ , and  $\eta$  is the dynamic viscosity coefficient.

### 4. Summary of Test Method

4.1 The time is measured for a fixed volume of liquid to flow under gravity through the capillary of a calibrated viscometer under a reproducible driving head and at a closely controlled and known temperature. The kinematic viscosity is the product of the measured flow time and the calibration constant of the viscometer.

#### 5. Significance and Use

5.1 Many petroleum products, and some non-petroleum materials, are used as lubricants, and the correct operation of the equipment depends upon the appropriate viscosity of the liquid being used. In addition, the viscosity of many petroleum fuels is important for the estimation of optimum storage, handling, and operational conditions. Thus, the accurate determination of viscosity is essential to many product specifications.

## 6. Apparatus

- 6.1 *Viscometers*—Use only calibrated viscometers of the glass capillary type, capable of being used to determine kinematic viscosity within the limits of the precision given in the precision section.
- 6.1.1 Viscometers listed in Table A1.1, whose specifications meet those given in Specifications D 446 and in ISO 3105 meet these requirements. It is not intended to restrict this test method

- to the use of only those viscometers listed in Table A1.1. Annex A1 gives further guidance.
- 6.1.2 Automation—Automated viscometers, which have been shown to determine kinematic viscosity within the limits of precision given in Section 16 are acceptable alternatives. Apply a kinetic energy correction (see Specifications D 446 and ISO 3105) to kinematic viscosities less than 10 mm<sup>2</sup>/s and flow times less than 200 s.
- 6.2 Viscometer Holders—Use viscometer holders to enable all viscometers which have the upper meniscus directly above the lower meniscus to be suspended vertically within  $1^{\circ}$  in all directions. Those viscometers whose upper meniscus is offset from directly above the lower meniscus shall be suspended vertically within  $0.3^{\circ}$  in all directions (see Specifications D 446 and ISO 3105).
- 6.2.1 Viscometers shall be mounted in the constant temperature bath in the same manner as when calibrated and stated on the certificate of calibration. See Specifications D 446, see Operating Instructions in Annex A1, Annex A2, and Annex A3. For those viscometers which have Tube L (see Specifications D 446) held vertical, vertical alignment shall be confirmed by using (*I*) a holder ensured to hold Tube L vertical, or (2) a bubble level mounted on a rod designed to fit into Tube L, or (*3*) a plumb line suspended from the center of Tube L, or (*4*) other internal means of support provided in the constant temperature bath.
- 6.3 Temperature-Controlled Bath—Use a transparent liquid bath of sufficient depth such, that at no time during the measurement of flow time, any portion of the sample in the viscometer is less than 20 mm below the surface of the bath liquid or less than 20 mm above the bottom of the bath.
- 6.3.1 Temperature Control—For each series of flow time measurements, the temperature control of the bath liquid shall be such that within the range from 15 to 100°C, the temperature of the bath medium does not vary by more than  $\pm 0.02$ °C of the selected temperature over the length of the viscometer, or between the position of each viscometer, or at the location of the thermometer. For temperatures outside this range, the deviation from the desired temperature must not exceed  $\pm$  0.05°C.
- 6.4 Temperature Measuring Device in the Range from 0 to  $100^{\circ}\text{C}$ —Use either calibrated liquid-in-glass thermometers (Annex A2) of an accuracy after correction of  $\pm 0.02^{\circ}\text{C}$  or better, or any other thermometric device of equal or better accuracy.
- 6.4.1 If calibrated liquid-in-glass thermometers are used, the use of two thermometers is recommended. The two thermometers shall agree within  $0.04^{\circ}$ C.
- 6.4.2 Outside the range from 0 to 100°C, use either calibrated liquid-in-glass thermometers of an accuracy after correction of  $\pm$  0.05°C or better, or any other thermometric device of equal or better accuracy. When two temperature measuring devices are used in the same bath, they shall agree within  $\pm$ 0.1°C.
- 6.4.3 When using liquid-in-glass thermometers, such as those in Table A2.2, use a magnifying device to read the thermometer to the nearest  $\frac{1}{5}$  division (for example, 0.01°C or 0.02°F) to ensure that the required test temperature and

temperature control capabilities are met (see 9.1). It is recommended that thermometer readings (and any corrections supplied on the certificates of calibrations for the thermometers) be recorded on a periodic basis to demonstrate compliance with the test method requirements. This information can be quite useful, especially when investigating issues or causes relating to testing accuracy and precision.

- 6.5 Timing Device—Use any timing device that is capable of taking readings with a discrimination of 0.1 s or better, and has an accuracy within  $\pm 0.07$  % (see Annex A3) of the reading when tested over intervals of 200 and 900 s.
- 6.5.1 Electrical timing devices may be used if the current frequency is controlled to an accuracy of 0.05 % or better. Alternating currents, as provided by some public power systems, are intermittently rather than continuously controlled. When used to actuate electrical timing devices, such control can cause large errors in kinematic viscosity flow time measurements.

# 7. Reagents and Materials

7.1 Chromic Acid Cleaning Solution, or a nonchromium-containing, strongly oxidizing acid cleaning solution.

Note 2—Warning: Chromic acid is a health hazard. It is toxic, a recognized carcinogen, highly corrosive, and potentially hazardous in contact with organic materials. If used, wear a full face-shield and full-length protective clothing including suitable gloves. Avoid breathing vapor. Dispose of used chromic acid carefully as it remains hazardous. Nonchromium-containing, strongly oxidizing acid cleaning solutions are also highly corrosive and potentially hazardous in contact with organic materials, but do not contain chromium which has special disposal problems.

- 7.2 *Sample Solvent*, completely miscible with the sample. Filter before use.
- 7.2.1 For most samples a volatile petroleum spirit or naphtha is suitable. For residual fuels, a prewash with an aromatic solvent such as toluene or xylene may be necessary to remove asphaltenic material.
- 7.3 *Drying Solvent*, a volatile solvent miscible with the sample solvent (see 7.2) and water (see 7.4). Filter before use.
  - 7.3.1 Acetone is suitable.
- 7.4 *Water*, deionized or distilled and conforming to Specification D 1193 or Grade 3 of ISO 3696. Filter before use.

#### 8. Calibration and Verification

- 8.1 *Viscometers*—Use only calibrated viscometers, thermometers, and timers as described in Section 6.
- 8.2 Certified Viscosity Reference Standards<sup>8</sup> (Table A1.2)—These are for use as confirmatory checks on the procedure in the laboratory.
- 8.2.1 If the determined kinematic viscosity does not agree within  $\pm~0.35$ % of the certified value, recheck each step in the procedure, including thermometer and viscometer calibration, to locate the source of error. Annex A1 gives details of standards available.
  - 8.2.2 The most common sources of error are caused by

<sup>8</sup> The ASTM Viscosity Oil Standards are available in 1-pt (0.47 L) containers. Purchase orders should be addressed to the Cannon Instrument Co., P.O. Box 16, State College, PA 16804. Shipment will be made as specified or by best means.

particles of dust lodged in the capillary bore and temperature measurement errors. It must be appreciated that a correct result obtained on a standard oil does not preclude the possibility of a counterbalancing combination of the possible sources of error.

8.3 The calibration constant, C, is dependent upon the gravitational acceleration at the place of calibration and this must, therefore, be supplied by the standardization laboratory together with the instrument constant. Where the acceleration of gravity, g, differs by more that 0.1 %, correct the calibration constant as follows:

$$C_2 = (g_2/g_1) \times C_1 \tag{1}$$

where the subscripts 1 and 2 indicate, respectively, the standardization laboratory and the testing laboratory.

# 9. General Procedure for Kinematic Viscosity

- 9.1 Adjust and maintain the viscometer bath at the required test temperature within the limits given in 6.3.1 taking account of the conditions given in Annex A2 and of the corrections supplied on the certificates of calibration for the thermometers.
- 9.1.1 Thermometers shall be held in an upright position under the same conditions of immersion as when calibrated.
- 9.1.2 In order to obtain the most reliable temperature measurement, it is recommended that two thermometers with valid calibration certificates be used (see 6.4).
- 9.1.3 They should be viewed with a lens assembly giving approximately five times magnification and be arranged to eliminate parallax errors.
- 9.2 Select a clean, dry, calibrated viscometer having a range covering the estimated kinematic viscosity (that is, a wide capillary for a very viscous liquid and a narrower capillary for a more fluid liquid). The flow time shall not be less than 200 s or the longer time noted in Specifications D 446.
- 9.2.1 The specific details of operation vary for the different types of viscometers listed in Table A1.1 The operating instructions for the different types of viscometers are given in Specifications D 446.
- 9.2.2 When the test temperature is below the dew point, affix loosely packed drying tubes to the open ends of the viscometer. The drying tubes must fit the design of the viscometer and not restrict the flow of the sample by pressures created in the instrument. Carefully flush the moist room air from the viscometer by applying vacuum to one of the drying tubes. Finally, before placing the viscometer in the bath, draw up the sample into the working capillary and timing bulb and allow to drain back as an additional safeguard against moisture condensing or freezing on the walls.
- 9.2.3 Viscometers used for silicone fluids, fluorocarbons, and other liquids which are difficult to remove by the use of a cleaning agent, shall be reserved for the exclusive use of those fluids except during their calibration. Subject such viscometers to calibration checks at frequent intervals. The solvent washings from these viscometers shall not be used for the cleaning of other viscometers.

# 10. Procedure for Transparent Liquids

10.1 Charge the viscometer in the manner dictated by the design of the instrument, this operation being in conformity

with that employed when the instrument was calibrated. If the sample contains solid particles, filter during charging through a (75- $\mu$ m) filter (see Specifications D 446). If the sample is thought or known to contain fibers or solid particles, filter through a 75  $\mu$ m screen, either prior to or during charging (see Specifications D 446).

- Note 3—To minimize the potential of particles passing through the filter from aggregating, it is recommended that the time lapse between filtering and charging be kept to a minimum.
- 10.1.1 In general, the viscometers used for transparent liquids are of the type listed in Table A1.1, A and B.
- 10.1.2 With certain products which exhibit *gel-like* behavior, exercise care that flow time measurements are made at sufficiently high temperatures for such materials to flow freely, so that similar kinematic viscosity results are obtained in viscometers of different capillary diameters.
- 10.1.3 Allow the charged viscometer to remain in the bath long enough to reach the test temperature. Where one bath is used to accommodate several viscometers, never add or withdraw a viscometer while any other viscometer is in use for measuring a flow time.
- 10.1.4 Because this time will vary for different instruments, for different temperatures, and for different kinematic viscosities, establish a safe equilibrium time by trial.
- 10.1.4.1 Thirty minutes should be sufficient except for the highest kinematic viscosities.
- 10.1.5 Where the design of the viscometer requires it, adjust the volume of the sample to the mark after the sample has reached temperature equilibrium.
- 10.2 Use suction (if the sample contains no volatile constituents) or pressure to adjust the head level of the test sample to a position in the capillary arm of the instrument about 7 mm above the first timing mark, unless any other value is stated in the operating instructions for the viscometer. With the sample flowing freely, measure, in seconds to within 0.1 s, the time required for the meniscus to pass from the first to the second timing mark. If this flow time is less than the specified minimum (see 9.2), select a viscometer with a capillary of smaller diameter and repeat the operation.
- 10.2.1 Repeat the procedure described in 10.2 to make a second measurement of flow time. Record both measurements.
- 10.2.2 If the two determinations of kinematic viscosity, calculated from the flow time measurements, agree within the stated determinability figure (see 16.1) for the product, use the average of these determinations to calculate the kinematic viscosity result to be reported. Record the result. If the determinations of kinematic viscosity do not agree within the stated determinability, repeat the measurements of flow times after thorough cleaning and drying of the viscometers and filtering (where required, see 10.1) of the sample. If the material or temperature, or both, is not listed in 16.1, for temperatures between 15 and 100°C use as an estimate of the determinability 0.20 %, and 0.35 % for temperatures outside this range.

#### 11. Procedure for Opaque Liquids

11.1 For steam-refined cylinder oils and black lubricating oils, proceed to 11.3 ensuring a thoroughly representative

- sample is used. The kinematic viscosity of residual fuel oils and similar waxy products can be affected by the previous thermal history and the following procedure described in 11.1.1-11.2.2 shall be followed to minimize this.
- 11.1.1 In general, the viscometers used for opaque liquids are of the reverse-flow type listed in Table A1.1, C.
- 11.1.2 Heat in the original container, in an oven, at 60  $\pm$  2°C for 1 h.
- 11.1.3 Thoroughly stir the sample with a suitable rod of sufficient length to reach the bottom of the container. Continue stirring until there is no sludge or wax adhering to the rod.
- 11.1.4 Recap the container tightly and shake vigorously for 1 min to complete the mixing.
- 11.1.4.1 With samples of a very waxy nature or oils of high kinematic viscosity, it may be necessary to increase the heating temperature above 60°C to achieve proper mixing. The sample should be sufficiently fluid for ease of stirring and shaking.
- 11.2 Immediately after completing 11.1.4, pour sufficient sample to fill two viscometers into a 100-mL glass flask and loosely stopper.
- 11.2.1 Immerse the flask in a bath of boiling water for 30 min.
- NOTE 4—**Precaution:** Exercise care as vigorous boil-over can occur when opaque liquids which contain high levels of water are heated to high temperatures.
- 11.2.2 Remove the flask from the bath, stopper tightly, and shake for 60 s.
- 11.3 Charge two viscometers in the manner dictated by the design of the instrument. For example, for the cross-arm or the BS U-tube viscometers for opaque liquids, filter the sample through a 75-µm filter into two viscometers previously placed in the bath. For samples subjected to heat treatment, use a preheated filter to prevent the sample coagulating during the filtration.
- 11.3.1 Viscometers which are charged before being inserted into the bath may need to be preheated in an oven prior to charging the sample. This is to ensure that the sample will not be cooled below test temperature.
- 11.3.2 After 10 min, adjust the volume of the sample (where the design of the viscometer requires) to coincide with the filling marks as in the viscometer specifications (see Specifications D 446).
- 11.3.3 Allow the charged viscometers enough time to reach the test temperature (see 11.3.1). Where one bath is used to accommodate several viscometers, never add or withdraw a viscometer while any other viscometer is in use for measuring flow time.
- 11.4 With the sample flowing freely, measure in seconds to within 0.1 s, the time required for the advancing ring of contact to pass from the first timing mark to the second. Record the measurement.
- 11.4.1 In the case of samples requiring heat treatment described in 11.1-11.2.1, complete the measurements of flow time within 1 h of completing 11.2.2. Record the measured flow times.
- 11.5 Calculate kinematic viscosity,  $\nu$ , in mm  $^2$ /s, from each measured flow time.
  - 11.5.1 For residual fuel oils, if the two determinations of

kinematic viscosity agree within the stated determinability figure (see 16.1), use the average of these determinations to calculate the kinematic viscosity result to be reported. Record the result. If the calculated kinematic viscosities do not agree, repeat the measurements of flow times after thorough cleaning and drying of the viscometers and filtering of the sample. If the material or temperature, or both, is not listed in 16.1, for temperatures between 15 and 100°C use as an estimate of the determinability 1.0 %, and 1.5 % for temperatures outside this range; it must be realized that these materials can be non-Newtonian, and can contain solids which can come out of solution as the flow time is being measured.

11.5.2 For other opaque liquids, no precision data is available.

# 12. Cleaning of Viscometer

- 12.1 Between successive determinations of kinematic viscosity, clean the viscometer thoroughly by several rinsings with the sample solvent, followed by the drying solvent (see 7.3). Dry the tube by passing a slow stream of filtered dry air through the viscometer for 2 min or until the last trace of solvent is removed.
- 12.2 Periodically clean the viscometer with the cleaning solution (**Warning**—see 7.1), for several hours to remove residual traces of organic deposits, rinse thoroughly with water (7.4) and drying solvent (see 7.3), and dry with filtered dry air or a vacuum line. Remove any inorganic deposits by hydrochloric acid treatment before the use of cleaning acid, particularly if the presence of barium salts is suspected.

Note 5—Caution: It is essential that alkaline cleaning solutions are not used as changes in the viscometer calibration can occur.

# 13. Calculation

13.1 Calculate the kinematic viscosity,  $\nu$ , from the measured flow time, t, and the viscometer constant, C, by means of the following equation:

$$\nu = C \cdot t \tag{2}$$

where:

 $\nu = \text{kinematic viscosity, mm}^2/\text{s},$ 

 $C = \text{calibration constant of the viscometer, } (\text{mm}^2/\text{s})/\text{s}, \text{ and}$ 

t = mean flow time, s.

13.2 Calculate the dynamic viscosity,  $\eta$ , from the calculated kinematic viscosity,  $\nu$ , and the density,  $\rho$ , by means of the following equation:

$$\eta = \nu \times \rho \times 10^{-3} \tag{3}$$

where:

 $\eta$  = dynamic viscosity, mPa·s,

ρ = density, kg/m³, at the same temperature used for the determination of the kinematic viscosity, and

 $\nu = \text{kinematic viscosity, mm}^2/\text{s.}$ 

13.2.1 The density of the sample can be determined at the test temperature of the kinematic viscosity determination by an appropriate method such as Test Methods D 1217, D 1480, or D 1481.

#### 14. Expression of Results

14.1 Report the test results for the kinematic or dynamic

viscosity, or both, to four significant figures, together with the test temperature.

# 15. Report

- 15.1 Report the following information:
- 15.1.1 Type and identification of the product tested,
- 15.1.2 Reference to this test method or a corresponding international standard,
  - 15.1.3 Result of the test (see Section 14),
- 15.1.4 Any deviation, by agreement or otherwise, from the procedure specified,
  - 15.1.5 Date of the test, and
  - 15.1.6 Name and address of the test laboratory.

#### 16. Precision

16.1 Determinability (d)—The difference between successive determinations obtained by the same operator in the same laboratory using the same apparatus for a series of operations leading to a single result, would in the long run, in the normal and correct operation of this test method, exceed the values indicated only in one case in twenty: $^{9,10,11}$ , $^{12,13,14,15,16}$ 

Base oils at 40 and 100°C9	0.0020 y	(0.20 %)
Formulated oils at 40 and 100°C <sup>10</sup>	0.0013 y	(0.13 %)
Formulated oils at 150°C <sup>11</sup>	0.015 y	(1.5 %)
Petroleum wax at 100°C <sup>12</sup>	0.0080 y	(0.80%)
Residual fuel oils at 80 and 100°C <sup>13</sup>	0.011 (y + 8)	
Residual fuel oils at 50°C <sup>13</sup>	0.017 y	(1.7 %)
Additives at 100°C <sup>14</sup>	0.00106 y <sup>1.1</sup>	
Gas oils at 40°C <sup>15</sup>	0.0013 (y+1)	
Jet fuels at −20°C <sup>16</sup>	0.0018 y	(0.18 %)

where: y is the average of determinations being compared. 16.2 Repeatability (r)—The difference between successive

<sup>14</sup> These precision values were obtained by statistical examination of interlaboratory results from eight additives in the range from 145 to 1500 mm²/s at 100°C and were first available in 1997. Precision data available from ASTM Headquarters. Request RR:D02-1421.

<sup>15</sup> These precision values were obtained by statistical examination of interlaboratory results from eight gas oils in the range from 1 to 13 mm<sup>2</sup>/s at 40°C and were first available in 1997. Precision data available from ASTM Headquarters. Request RR:D02-1422.

 $^{16}$  These precision values were obtained by statistical examination of interlaboratory results from nine jet fuels in the range from 4.3 to 5.6 mm  $^2/s$  at–  $20^{\circ}C$  and were first available in 1997. Precision data available from ASTM Headquarters. Request RR:D02-1420.

<sup>&</sup>lt;sup>9</sup> These precision values were obtained by statistical examination of interlaboratory results from six mineral oils (base oils without additive package) in the range from 8 to 1005 mm²/s at 40°C and from 2 to 43 mm²/s at 100°C, and were first published in 1989. Precision data available from ASTM Headquarters. Request RR:D02-1331 and RR:D02-1132. See Guide D 6074.

 $<sup>^{10}</sup>$  These precision values were obtained by statistical examination of interlaboratory results from seven fully formulated engine oils in the range from 36 to 340  $\,$  mm²/s at  $40^{\circ}$ C and from 6 to 25 mm²/s at  $100^{\circ}$ C, and were first published in 1991. Precision data available from ASTM Headquarters. Request RR:D02-1332. See Guide D 6071.

 $<sup>^{11}</sup>$  These precision values were obtained by statistical examination of interlaboratory results for eight fully formulated engine oils in the range from 7 to 19 mm  $^2/s$  at  $150^{\circ}\text{C}$ , and first published in 1991. Precision data available from ASTM Headquarters. Request RR:D02-1333. See Guide D 6074.

 $<sup>^{12}</sup>$  These precision values were obtained by statistical examination of interlaboratory results from five petroleum waxes in the range from 3 to 16  $\rm mm^2/s$  at  $100^{\circ}\rm C$ , and were first published in 1988. Precision data available from ASTM Headquarters. Request RR:D02-1334.

<sup>&</sup>lt;sup>13</sup> These precision values were obtained by statistical examination of interlaboratory results from fourteen residual fuel oils in the range from 30 to 1300 mm <sup>2</sup>/s at 50°C and from 5 to 170 mm<sup>2</sup>/s at 80 and 100°C, and were first published in 1984. Precision data available from ASTM Headquarters. Request RR:D02-1198.



results obtained by the same operator in the same laboratory with the same apparatus under constant operating conditions on identical test material would, in the long run, in the normal and correct operation of this test method, exceed the values indicated only in one case in twenty:<sup>9,10,11</sup>, 12,13,14,15,16

Base oils at 40 and 100°C9	0.0011 x	(0.11 %)
Formulated oils at 40 and 100°C <sup>10</sup>	0.0026 x	(0.26 %)
Formulated oils at 150°C <sup>11</sup>	0.0056 x	(0.56 %)
Petroleum wax at 100°C <sup>12</sup>	0.0141 x <sup>1.2</sup>	
Residual fuel oils at 80 and 100°C <sup>13</sup>	0.013 (x + 8)	
Residual oils at 50°C <sup>13</sup>	0.015 x	(1.5 %)
Additives at 100°C <sup>14</sup>	0.00192 x <sup>1.1</sup>	
Gas oils at 40°C15	0.0043 (x+1)	
Jet fuels at −20°C <sup>16</sup>	0.007 x	(0.7 %)

where: x is the average of results being compared.

16.3 Reproducibility (R)—The difference between two single and independent results obtained by different operators working in different laboratories on nominally identical test material would, in the long run, in the normal and correct operation of this test method, exceed the values indicated

below only in one case in twenty.9,10,11,12,13,14,15,16

Base oils at 40 and 100°C9	0.0065 x	(0.65 %)
Formulated oils at 40 and 100°C	0.0076 x	(0.76 %)
Formulated oils at 150°C <sup>11</sup>	0.018 x	(1.8 %)
Petroleum wax at 100°C <sup>12</sup>	0.0366 x <sup>1.2</sup>	
Residual fuel oils at 80 and 100°C <sup>13</sup>	0.04 (x + 8)	
Residual oils at 50°C <sup>13</sup>	0.074 x	(7.4 %)
Additives at 100°C <sup>14</sup>	0.00862 x <sup>1.1</sup>	
Gas oils at 40°C <sup>15</sup>	0.0082 (x+1)	
Jet fuels at −20°C <sup>16</sup>	0.019 x	(1.9 %)

where: x is the average of results being compared.

16.4 The precision for used oils has not been determined but is expected to be poorer than that for formulated oils. Because of the extreme variability of such used oils, it is not anticipated that the precision of used oils will be determined.

#### 17. Keywords

17.1 dynamic viscosity; kinematic viscosity; viscometer; viscosity

#### **ANNEXES**

(Mandatory Information)

# A1. VISCOMETER TYPES, CALIBRATION, AND VERIFICATION

#### **A1.1 Viscometer Types**

A1.1.1 Table A1.1 lists capillary viscometers commonly in use for viscosity determinations on petroleum products. For specifications and operating instructions, refer to Specifications D 446.

**TABLE A1.1 Viscometer Types** 

Viscometer Identification         Kinematic Viscosity Range, Amm²/s           A. Ostwald Types for Transparent Liquids           Cannon-Fenske routine BS/U-fuchs         0.5 to 20 000           Zeitfuchs         0.6 to 3 000           BS/U-tube BS/U-fuchs         0.9 to 10 000           BS/U-M miniature         0.2 to 100           SIL BS/U-fuchs         0.6 to 10 000           Cannon-Manning semi-micro         0.4 to 20 000           Pinkevitch BS/IP/SL BS/IP/SL(S) BS/IP/SL	TABLE AT.1 Viscometer Types						
Cannon-Fenske routine <sup>8</sup> Cannon-Fenske routine <sup>8</sup> D.5 to 20 000  Zeitfuchs  D.6 to 3 000  BS/U-tube <sup>8</sup> D.9 to 10 000  BS/U/M miniature  D.2 to 100  SIL <sup>8</sup> D.6 to 10 000  Cannon-Manning semi-micro  D.4 to 20 000  Pinkevitch <sup>8</sup> D.6 to 17 000  B. Suspended-level Types for Transparent Liquids  BS/IP/SL <sup>8</sup> D.6 to 100 000  BS/IP/SL(S) <sup>8</sup> D.5 to 100 000  BS/IP/MSL  D.6 to 3 000  Ubbelohde <sup>8</sup> D.3 to 100 000  FitzSimons  D.6 to 1 200  Atlantic <sup>8</sup> D.75 to 5 000  Cannon-Ubbelohde (A), Cannon  D.5 to 100 000  Ubbelohde dilution <sup>8</sup> (B)  Cannon-Ubbelohde semi-micro  C. Reverse-flow Types for Transparent and Opaque Liquids  Cannon-Fenske opaque  D.4 to 20 000  Zeitfuchs cross-arm  D.6 to 100 000  Zeitfuchs cross-arm  D.6 to 100 000  Estiruchs cross-arm  D.6 to 300 000	Viscometer Identification	Kinematic Viscosity Range, A mm <sup>2</sup> /s					
Zeitfuchs         0.6         to 3000           BS/U-tube <sup>β</sup> 0.9         to 10000           BS/U/M miniature         0.2         to 100           SIL <sup>B</sup> 0.6         to 10000           Cannon-Manning semi-micro         0.4         to 20000           Pinkevitch <sup>B</sup> 0.6         to 17000           B. Suspended-level Types for Transparent Liquids           BS/IP/SL <sup>B</sup> 3.5         to 100 000           BS/IP/SL(S) <sup>B</sup> 1.05 to 100 000           BS/IP/MSL         0.6         to 3000           Ubbelohde <sup>B</sup> 0.3 to 100 000           FitzSimons         0.6 to 1 200           Atlantic <sup>B</sup> 0.75 to 5 000           Cannon-Ubbelohde(A), Cannon         0.5 to 100 000           Ubbelohde dilution <sup>B</sup> (B)         0.4 to 20 000           C. Reverse-flow Types for Transparent and Opaque Liquids           Cannon-Fenske opaque         0.4 to 20 000           Zeitfuchs cross-arm         0.6 to 100 000           BS/IP/RF U-tube reverse-flow         0.6 to 300 000	A. Ostwald Types for Transparent Liquids						
BS/IJ-tube <sup>B</sup> 0.9 to 10 000 BS/U/M miniature 0.2 to 100 SIL <sup>B</sup> 0.6 to 10 000 Cannon-Manning semi-micro 0.4 to 20 000 Pinkevitch <sup>B</sup> 0.6 to 17 000  B. Suspended-level Types for Transparent Liquids  BS/IP/SL <sup>B</sup> 3.5 to 100 000 BS/IP/SL(S) <sup>B</sup> 1.05 to 10 000 BS/IP/MSL 0.6 to 3 000 Ubbelohde <sup>B</sup> 0.3 to 100 000 FitzSimons 0.6 to 1 200 Atlantic <sup>B</sup> 0.75 to 5 000 Cannon-Ubbelohde(A), Cannon 0.5 to 100 000 Ubbelohde dilution <sup>B</sup> (B) Cannon-Ubbelohde semi-micro 0.4 to 20 000  C. Reverse-flow Types for Transparent and Opaque Liquids  Cannon-Fenske opaque 0.4 to 20 000 Zeitfuchs cross-arm 0.6 to 100 000 BS/IP/RF U-tube reverse-flow 0.6 to 300 000	Cannon-Fenske routine <sup>B</sup>	0.5 to 20 000					
BS/U/M miniature	Zeitfuchs	0.6 to 3 000					
SILB         0.6 to 10 000           Cannon-Manning semi-micro         0.4 to 20 000           Pinkevitch         0.6 to 17 000           B. Suspended-level Types for Transparent Liquids           BS/IP/SLB         3.5 to 100 000           BS/IP/SL(S)B         1.05 to 10 000           BS/IP/MSL         0.6 to 3 000           UbbelohdeB         0.3 to 100 000           FitzSimons         0.6 to 1 200           AtlanticB         0.75 to 5 000           Cannon-Ubbelohde(A), Cannon         0.5 to 100 000           Ubbelohde dilutionB(B)         0.4 to 20 000           C. Reverse-flow Types for Transparent and Opaque Liquids           Cannon-Fenske opaque         0.4 to 20 000           Zeitfuchs cross-arm         0.6 to 100 000           BS/IP/RF U-tube reverse-flow         0.6 to 300 000	BS/U-tube <sup>B</sup>	0.9 to 10 000					
Cannon-Manning semi-micro         0.4 to 20 000           Pinkevitch <sup>B</sup> 0.6 to 17 000           B. Suspended-level Types for Transparent Liquids           BS/IP/SL <sup>B</sup> 3.5 to 100 000           BS/IP/SL(S) <sup>B</sup> 1.05 to 10 000           BS/IP/MSL         0.6 to 3 000           Ubbelohde <sup>B</sup> 0.3 to 100 000           FitzSimons         0.6 to 1 200           Atlantic <sup>B</sup> 0.75 to 5 000           Cannon-Ubbelohde(A), Cannon         0.5 to 100 000           Ubbelohde dilution <sup>B</sup> (B)         0.4 to 20 000           Cannon-Ubbelohde semi-micro         0.4 to 20 000           Cannon-Fenske opaque         0.4 to 20 000           Zeitfuchs cross-arm         0.6 to 100 000           BS/IP/RF U-tube reverse-flow         0.6 to 300 000	BS/U/M miniature	0.2 to 100					
Pinkevitch <sup>B</sup> 0.6 to 17 000           B. Suspended-level Types for Transparent Liquids           BS/IP/SL <sup>B</sup> 3.5 to 100 000           BS/IP/SL(S) <sup>B</sup> 1.05 to 10 000           BS/IP/MSL         0.6 to 3 000           Ubbelohde <sup>B</sup> 0.3 to 100 000           FitzSimons         0.6 to 1 200           Atlantic <sup>B</sup> 0.75 to 5 000           Cannon-Ubbelohde(A), Cannon         0.5 to 100 000           Ubbelohde dilution <sup>B</sup> (B)         0.4 to 20 000           Cannon-Ubbelohde semi-micro         0.4 to 20 000           Cannon-Fenske opaque         0.4 to 20 000           Zeitfuchs cross-arm         0.6 to 100 000           BS/IP/RF U-tube reverse-flow         0.6 to 300 000	$SIL^B$	0.6 to 10 000					
B. Suspended-level Types for Transparent Liquids  BS/IP/SL <sup>B</sup> 3.5 to 100 000  BS/IP/SL(S) <sup>B</sup> 1.05 to 10 000  BS/IP/MSL 0.6 to 3 000  Ubbelohde <sup>B</sup> 0.3 to 100 000  FitzSimons 0.6 to 1 200  Atlantic <sup>B</sup> 0.75 to 5 000  Cannon-Ubbelohde(A), Cannon 0.5 to 100 000  Ubbelohde dilution <sup>B</sup> (B)  Cannon-Ubbelohde semi-micro 0.4 to 20 000  C. Reverse-flow Types for Transparent and Opaque Liquids  Cannon-Fenske opaque 0.4 to 20 000  Zeitfuchs cross-arm 0.6 to 100 000  BS/IP/RF U-tube reverse-flow 0.6 to 300 000	Cannon-Manning semi-micro	0.4 to 20 000					
BS/IP/SL <sup>B</sup> BS/IP/SL(S) <sup>B</sup> 1.05 to 100 000  BS/IP/MSL  0.6 to 3 000  Ubbelohde <sup>B</sup> 0.3 to 100 000  FitzSimons  0.6 to 1 200  Atlantic <sup>B</sup> 0.75 to 5 000  Cannon-Ubbelohde(A), Cannon  0.5 to 100 000  Ubbelohde dilution <sup>B</sup> (B)  Cannon-Ubbelohde semi-micro  0.4 to 20 000  C. Reverse-flow Types for Transparent and Opaque Liquids  Cannon-Fenske opaque  0.4 to 20 000  Zeitfuchs cross-arm  0.6 to 100 000  BS/IP/RF U-tube reverse-flow  0.6 to 300 000	Pinkevitch <sup>B</sup>	0.6 to 17 000					
BS/IP/SL(S) <sup>B</sup> 1.05 to 10 000 BS/IP/MSL 0.6 to 3 000 Ubbelohde <sup>B</sup> 0.3 to 100 000 FitzSimons 0.6 to 1 200 Atlantic <sup>B</sup> 0.75 to 5 000 Cannon-Ubbelohde(A), Cannon 0.5 to 100 000 Ubbelohde dilution <sup>B</sup> (B) Cannon-Ubbelohde semi-micro 0.4 to 20 000  C. Reverse-flow Types for Transparent and Opaque Liquids  Cannon-Fenske opaque 0.4 to 20 000 Zeitfuchs cross-arm 0.6 to 100 000 BS/IP/RF U-tube reverse-flow 0.6 to 300 000	B. Suspended-level Ty	pes for Transparent Liquids					
BS/IP/MSL       0.6 to 3 000         Ubbelohde <sup>B</sup> 0.3 to 100 000         FitzSimons       0.6 to 1 200         Atlantic <sup>B</sup> 0.75 to 5 000         Cannon-Ubbelohde(A), Cannon       0.5 to 100 000         Ubbelohde dilution <sup>B</sup> (B)       0.4 to 20 000         Cannon-Ubbelohde semi-micro       0.4 to 20 000         C. Reverse-flow Types for Transparent and Opaque Liquids         Cannon-Fenske opaque       0.4 to 20 000         Zeitfuchs cross-arm       0.6 to 100 000         BS/IP/RF U-tube reverse-flow       0.6 to 300 000	BS/IP/SL <sup>B</sup>	3.5 to 100 000					
Ubbelohde <sup>B</sup> 0.3 to 100 000  FitzSimons 0.6 to 1 200  Atlantic <sup>B</sup> 0.75 to 5 000  Cannon-Ubbelohde(A), Cannon 0.5 to 100 000  Ubbelohde dilution <sup>B</sup> (B)  Cannon-Ubbelohde semi-micro 0.4 to 20 000  C. Reverse-flow Types for Transparent and Opaque Liquids  Cannon-Fenske opaque 0.4 to 20 000  Zeitfuchs cross-arm 0.6 to 100 000  BS/IP/RF U-tube reverse-flow 0.6 to 300 000	BS/IP/SL(S) <sup>B</sup>	1.05 to 10 000					
FitzSimons         0.6 to 1 200           Atlantic <sup>B</sup> 0.75 to 5 000           Cannon-Ubbelohde(A), Cannon         0.5 to 100 000           Ubbelohde dilution <sup>B</sup> (B)         0.4 to 20 000           Cannon-Ubbelohde semi-micro         0.4 to 20 000           C. Reverse-flow Types for Transparent and Opaque Liquids           Cannon-Fenske opaque         0.4 to 20 000           Zeitfuchs cross-arm         0.6 to 100 000           BS/IP/RF U-tube reverse-flow         0.6 to 300 000	BS/IP/MSL	0.6 to 3 000					
Atlantic <sup>B</sup> 0.75 to 5 000 Cannon-Ubbelohde(A), Cannon 0.5 to 100 000 Ubbelohde dilution <sup>B</sup> (B) Cannon-Ubbelohde semi-micro 0.4 to 20 000  C. Reverse-flow Types for Transparent and Opaque Liquids  Cannon-Fenske opaque 0.4 to 20 000  Zeitfuchs cross-arm 0.6 to 100 000 BS/IP/RF U-tube reverse-flow 0.6 to 300 000	Ubbelohde <sup>B</sup>	0.3 to 100 000					
Cannon-Ubbelohde (A), Cannon         0.5 to 100 000           Ubbelohde dilution B(B)         0.4 to 20 000           Cannon-Ubbelohde semi-micro         0.4 to 20 000           C. Reverse-flow Types for Transparent and Opaque Liquids           Cannon-Fenske opaque         0.4 to 20 000           Zeitfuchs cross-arm         0.6 to 100 000           BS/IP/RF U-tube reverse-flow         0.6 to 300 000	FitzSimons	0.6 to 1 200					
Ubbelohde dilution <sup>B</sup> (B)           Cannon-Ubbelohde semi-micro         0.4 to 20 000           C. Reverse-flow Types for Transparent and Opaque Liquids           Cannon-Fenske opaque         0.4 to 20 000           Zeitfuchs cross-arm         0.6 to 100 000           BS/IP/RF U-tube reverse-flow         0.6 to 300 000	Atlantic <sup>B</sup>	0.75 to 5 000					
Cannon-Ubbelohde semi-micro 0.4 to 20 000  C. Reverse-flow Types for Transparent and Opaque Liquids  Cannon-Fenske opaque 0.4 to 20 000  Zeitfuchs cross-arm 0.6 to 100 000  BS/IP/RF U-tube reverse-flow 0.6 to 300 000	Cannon-Ubbelohde(A), Cannon	0.5 to 100 000					
C. Reverse-flow Types for Transparent and Opaque Liquids  Cannon-Fenske opaque 0.4 to 20 000  Zeitfuchs cross-arm 0.6 to 100 000  BS/IP/RF U-tube reverse-flow 0.6 to 300 000	Ubbelohde dilution <sup>B</sup> (B)						
Cannon-Fenske opaque         0.4 to 20 000           Zeitfuchs cross-arm         0.6 to 100 000           BS/IP/RF U-tube reverse-flow         0.6 to 300 000	Cannon-Ubbelohde semi-micro	0.4 to 20 000					
Zeitfuchs cross-arm 0.6 to 100 000 BS/IP/RF U-tube reverse-flow 0.6 to 300 000	C. Reverse-flow Types for Transparent and Opaque Liquids						
BS/IP/RF U-tube reverse-flow 0.6 to 300 000	Cannon-Fenske opaque	0.4 to 20 000					
	Zeitfuchs cross-arm	0.6 to 100 000					
Lantz-Zeitfuchs type reverse-flow 60 to 100 000	BS/IP/RF U-tube reverse-flow	0.6 to 300 000					
	Lantz-Zeitfuchs type reverse-flow	60 to 100 000					

<sup>&</sup>lt;sup>A</sup>Each range quoted requires a series of viscometers. To avoid the necessity of making a kinetic energy correction, these viscometers are designed for a flow time in excess of 200 s except where noted in Specifications D 446.

#### A1.2 Calibration

A1.2.1 Calibrate working standard viscometers against master viscometers having a certificate of calibration traceable to a national standard. Viscometers used for analysis shall be calibrated in comparison with working standard viscometers or master viscometers, or by the procedures given in Specifications D 446 or ISO 3105. Viscometer constants shall be measured and expressed to the nearest 0.1 % of their value.

#### A1.3 Verification

A1.3.1 Viscometer constants shall either be verified by a similar procedure to A1.2, or conveniently checked by means of certified viscosity oils.

A1.3.2 These oils can be used for confirmatory checks on the procedure in a laboratory. If the measured viscosity does

TABLE A1.2 Viscosity Oil Standards<sup>A</sup>

Designation	Approximate Kinematic Viscosity, mm <sup>2</sup> /s					
Designation	-40°C	20°C	25°C	40°C	50°C	100°C
S3	80	4.6	4.0	2.9		1.2
S6		11	8.9	5.7		1.8
S20		44	34	18		3.9
S60		170	120	54		7.2
S200		640	450	180		17
S600		2 400	1 600	520	280	32
S2 000		8 700	5 600	1 700		75
S8 000		37 000	23 000	6 700		
S30 000			81 000	23 000	11 000	

<sup>&</sup>lt;sup>A</sup>The actual values for these standards are established and annually reaffirmed by cooperative tests. In 1991, tests were made using 15 different types of viscometers in 28 laboratories located in 14 countries.

 $<sup>^{\</sup>it B}$  In each of these series, the minimum flow time for the viscometers with lowest constants exceeds 200 s.

<sup>&</sup>lt;sup>B</sup> Kinematic viscosities may also be supplied at 100°F.

<sup>&</sup>lt;sup>C</sup> Kinematic viscosities may also be supplied at 210°F.



not agree within  $\pm$  0.35 % of the certified value, recheck each step in the procedure including thermometer, timer, and viscometer calibration to locate the source of error. It should be appreciated that a correct result obtained on a certified oil does not preclude the possibility of a counterbalancing combination of the possible sources of error.

A1.3.2.1 A range of viscosity oil standards is commercially available, and each oil carries a certification of the measured value established by multiple testing. Table A1.2 gives the standard range of oils, together with the approximate viscosities over a range of temperatures.

#### A2. KINEMATIC VISCOSITY TEST THERMOMETERS

# **A2.1 Short-Range Specialized Thermometer**

A2.1.1 Use a short-range specialized thermometer conforming to the generic specification given in Table A2.1 and Table A2.2 and to one of the designs shown in Fig. A2.1.

A2.1.2 The difference in the designs rests mainly in the position of the ice point scale. In Design A, the ice point is within the scale range, in Design B, the ice point is below the scale range, and in Design C, the ice point is above the scale range.

#### A2.2 Calibration

A2.2.1 Use liquid-in-glass thermometers with an accuracy after correction of 0.02°C or better, calibrated by a laboratory meeting the requirements of ISO 9000 or ISO 25, and carrying certificates confirming that the calibration is traceable to a national standard. As an alternative, use thermometric devices such as platinum resistance thermometers, of equal or better accuracy, with the same certification requirements.

A2.2.2 The scale correction of liquid-in-glass thermometers can change during storage and use, and therefore regular re-calibration is required. This is most conveniently achieved in a working laboratory by means of a re-calibration of the ice point, and all of the main scale corrections altered for the change seen in the ice point.

A2.2.2.1 It is recommended that the interval for ice-point checking be not greater than six months, but for new thermometers, monthly checking for the first six months is recommended. A complete new re-calibration of the thermometer, while permitted, is not necessary in order to meet the accuracy

**TABLE A2.1 General Specification for Thermometers** 

Note 1—Table A2.2 gives a range of ASTM, IP, and ASTM/IP thermometers that comply with the specification in Table A2.1, together with their designated test temperatures. See Specification E 1 and Test Method E 77.

Immersion		Total
Scale marks:		
Subdivisions	°C	0.05
Long lines at each	°C	0.1 and 0.5
Numbers at each	°C	1
Maximum line width	mm	0.10
Scale error at test temperature, max	°C	0.1
Expansion chamber:		
Permit heating to	°C	105 up to 90, 120 between 90 and 95
		130 between 95 and 105, 170 above
		105
Total length	mm	300 to 310
Stem outside diameter	mm	6.0 to 8.0
Bulb length	mm	45 to 55
Bulb outside diameter	mm	no greater than stem
Length of scale range	mm	40 to 90

**TABLE A2.2 Complying Thermometers** 

Thermometer No.	Te Tempe		Thermometer No.	Test Temperature	
	°C	°F	_	°C	°F
ASTM 132C, IP 102C	150		ASTM 128C, F/IP 33C	0	32
ASTM 110C, F/IP 93C	135	275	ASTM 72C, F/IP 67C	-17.8	0
ASTM 121C/IP 32C	98.9,	210,	ASTM 127C/IP 99C	-20	-4
	100	212	ASTM 126C, F/IP 71C	-26.1	-20
ASTM 129C, F/IP 36C	93.3	200	ASTM 73C, F/IP 68C	-40	-40
ASTM 48C, F/IP 90C IP 100C	82.2 80	180	ASTM 74C, F/IP 69C	-53.9	-65
ASTM 47C, F/IP 35C	60	140			
ASTM 29C, F/IP 34C	54.4	130			
ASTM 46C F/IP 66C	50	122			
ASTM 120C/IP 92C	40				
ASTM 28C, F/IP 31C	37.8	100			
ASTM 118C, F	30	86			
ASTM 45C, F/IP 30C	25	77			
ASTM 44C, F/IP 29C	20	68			

ascribed to this design thermometer until the ice-point change from the last full calibration amounts to one scale division, or more than five years have elapsed since the last full calibration.

A2.2.2.2 Other thermometric devices, if used, will also require periodic recalibration. Keep records of all recalibration.

A2.2.3 Procedure for Ice-point Re-calibration of Liquid-inglass Thermometers.

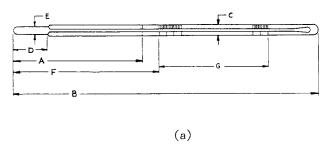
A2.2.3.1 Unless otherwise listed on the certificate of calibration, the re-calibration of calibrated kinematic viscosity thermometers requires that the ice-point reading shall be taken within 60 min after being at test temperature for not less than 3 min.

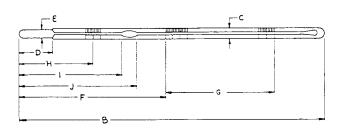
A2.2.3.2 Select clear pieces of ice, preferably made from distilled or pure water. Discard any cloudy or unsound portions. Rinse the ice with distilled water and shave or crush into small pieces, avoiding direct contact with the hands or any chemically unclean objects. Fill the Dewar vessel with the crushed ice and add sufficient water to form a slush, but not enough to float the ice. As the ice melts, drain off some of the water and add more crushed ice. Insert the thermometer, and pack the ice gently about the stem, to a depth approximately one scale division below the 0°C graduation.

A2.2.3.3 After at least 3 min have elapsed, tap the thermometer gently and repeatedly at right angles to its axis while making observations. Successive readings taken at least 1 min apart shall agree within 0.005°C.

A2.2.3.4 Record the ice-point readings and determine the thermometer correction at this temperature from the mean reading. If the correction is found to be higher or lower than







(b)

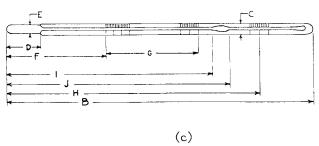


FIG. A2.1 Thermometer Designs

that corresponding to a previous calibration, change the correction at all other temperatures by the same value.

# A3. TIMER ACCURACY

\/\/\/H

- A3.1 Regularly check timers for accuracy and maintain records of such checks.
- A3.1.1 Time signals as broadcast by the National Institute of Standards and Technology are a convenient and primary standard reference for calibrating timing devices. The following can be used to an accuracy of 0.1 s:

WWV Fort Collins, CO 2.5, 5, 10, 15, 20 MHz

- A2.2.3.5 During the procedure, apply the following conditions:
  - (a) The thermometer shall be supported vertically.
- (b) View the thermometer with an optical aid that gives a magnification of approximately five and also eliminates parallax.
  - (c) Express the ice-point reading to the nearest 0.005°C.
- A2.2.4 When in use, immerse the thermometric device to the same depth as when it was fully calibrated. For example, if a liquid-in-glass thermometer was calibrated at the normal total immersion condition, it shall be immersed to the top of the mercury column with the remainder of the stem and the expansion volume at the uppermost end exposed to room temperature and pressure. In practice, this means that the top of the mercury column shall be within a length equivalent to four scale divisions of the surface of the medium whose temperature is being measured.
- A2.2.4.1 If this condition cannot be met, then an extra correction may be necessary.

CHU Ottawa, Canada 3.33, 7.335, 14.67 MHz

2.5, 5, 10, 15, MHz

Kauai, HI

A3.1.2 Radio broadcast of voice and audio on a telephone line at phone 303-499-7111. Additional time services are available from the National Institute of Standards and Technology.



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